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Journal article

**Event-triggered output feedback containment control for a class of stochastic nonlinear multi-agent systems**

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1 **Event-triggered output feedback containment**  
2 **control for a class of stochastic nonlinear multi-agent**  
3 **systems**

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8 **Abstract** An output feedback-based containment control strategy is proposed  
9 with an event-triggered mechanism for a class of stochastic nonlinear multi-  
10 agent systems (MASs). For unavailable internal states of individual agent, a  
11 state observer is constructed for their estimations. The dynamic surface control  
12 (DSC) technology is employed to improve traditional backstepping, where a  
13 first-order filter is introduced for derivation calculation of virtual control laws.  
14 For the purpose of reducing communication resources, a fixed threshold-based  
15 triggered strategy is presented to reduce data transmission bits over commu-  
16 nication channels. It is proven that all signals in the closed-loop system are  
17 bounded in probability and the containment control is achieved. Finally, the  
18 effectiveness of the proposed control strategy is verified via two examples.

19 **Keywords** Containment · Dynamic surface · Event-triggered · Neural  
20 networks · Stochastic multi-agent systems

21 **1 Introduction**

22 In the past decades, cooperative control of multi-agent systems (MASs) [1, 2, 3]  
23 has drawn large amounts of attentions. As one of critical issues in MASs'  
24 cooperative control [4, 5, 6], containment control makes followers remain in  
25 a convex hull spanned by leaders' information. It is applied in various fields  
26 in engineering, for instance, ship navigation, satellite attitude and unmanned  
27 aerial vehicles (UAVs) [7].

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28 Many efforts have been taken in containment control of MASs [8]. A linear  
29 scheme of containment control for MASs with switching communication topol-  
30 ogy problem is proposed [9]. MASs' dynamics in [10][11] are completely known.  
31 Owing to uncertain factors in many real applications, modeling agents with  
32 high accuracy is hard to achieve. The designed containment controllers should  
33 be equipped to adaptive algorithms to deal with uncertainties. In the existing  
34 works [12][13], random disturbances are ignored. Containment control for an  
35 MAS is discussed and a containment control scheme maintaining connectiv-  
36 ity is presented [14]. In [15], authors simplify formation containment control  
37 problems of UAVs and put forward sufficient conditions to keep formation  
38 containment through state transformation and state space decomposition. Be-  
39 sides, [16] presents a singularity-free adaptive fuzzy fixed-time control scheme  
40 by establishing a new error conversion mechanism and designing a barrier Lya-  
41 punov function. By a reinforcement learning algorithm, authors in [17] report  
42 an adaptive fault-tolerant tracking control problem, and they effectively re-  
43 duce the computational burden. In [18], Dong studies a containment control  
44 problem of MASs with time delays. From the viewpoint of the system feed-  
45 back, the above results mainly focus on state feedback control. Nevertheless,  
46 in the real world, it is difficult to measure the internal states directly due to  
47 technological limitations of measurement and economical factors.

48 Output schemes are feasible solutions for containment control. For the  
49 distribute containment control of high-order nonlinear MASs with a directed  
50 topology, an observer is constructed to estimate unmeasurable state variables,  
51 and an output feedback containment control law is proposed to steer the fol-  
52 lowers' states converge to a convex hull spanned by leaders' trajectories [19].  
53 A containment control law based on observer is proposed for nonlinear MASs  
54 with uncertainties [20]. In [21], an uncertain nonlinear strict feedback system  
55 is studied and a fuzzy containment control method with unmeasurable states  
56 is presented.

57 Apart from time-driven schemes, event-triggered mechanisms [22, 23, 24,  
58 25] are alternative in MAS control. A containment control problem with a  
59 trigger is solved in a directed topology [26]. A kind of triggered mechanisms  
60 determines updated instants, and it effectively saves communication resources  
61 over networks [27, 28]. In the framework of backstepping control, an adap-  
62 tive event-triggered consensus scheme [29] is developed for an MAS with an  
63 undirected graph. An event-triggered containment control strategy of MASs  
64 with external disturbances is studied [30]. For a consensus problem of MASs  
65 with general linear dynamics, a distributed and asynchronous event-triggered  
66 control strategy is proposed [31]. Finite time consensus control for MASs is  
67 reported [32], and a distributed event-triggered control strategy is presented.  
68 A polynomial event-triggered strategy is proposed to determine signal trans-  
69 mission, and a fault detection problem of nonlinear discrete time network  
70 system is addressed under event-triggered mechanism [33]. In [34], an aperi-  
71 odic event-triggered strategy is proposed, and stochastic nonlinear systems  
72 with unmeasurable states are in an undirected graph. Recently, for a class of  
73 output-constrained uncertain nonlinear MASs, authors in [35] present a novel

74 adaptive event-triggered control strategy on the basis of observers. In [36],  
 75 an event-triggered strategy with a varying threshold is proposed for nonaffine  
 76 pure-feedback MASs to reduce communication burdens.

77 In this paper, we focus attention on a class of stochastic nonlinear MASs  
 78 [37, 38]. For unavailable internal states of individual agent, state observers are  
 79 constructed, and a triggered strategy is proposed based on a fixed threshold.  
 80 The main contributions in this paper are listed as follows.

81 1) An event-trigger-based containment control strategy is proposed for a  
 82 stochastic nonlinear MASs with uncertainties. Different from most existing  
 83 results [39][40][41], whose control plants are deterministic MASs, stochastic  
 84 nonlinear ones are taken into account here. We are devoted to study the  
 85 containment control of stochastic nonlinear MASs based on event-triggered  
 86 mechanism, which is more applicable in practice. Only as a triggered condi-  
 87 tion is violated, control signal is transmitted via a communication channel.  
 88 The control strategy in our paper reduces the resource occupation of network  
 89 channels, and the number of data transmission bits over channels is reduced  
 90 by this triggered mechanism.

91 2) A first-order filter is introduced for a stochastic nonlinear MAS with un-  
 92 certain dynamics. Unlike [42], this paper studies DSC method for stochastic  
 93 nonlinear MASs with completely uncertain dynamics. It avoids explosion of  
 94 complexity in backstepping method [43], which needs large amount of calcula-  
 95 tion. In our paper, we can complete the complex derivation process by simple  
 96 algebraic operation. Also, a compensator is designed for a class of stochastic  
 97 nonlinear MASs with uncertain parameters to eliminate the influence of out-  
 98 put error which produced by a first-order filter. Compared with the result in  
 99 [44], the influence from a containment error is reduced, and the containment  
 100 performance of the system is improved in our paper.

101 The rest of this paper is organized as below. Section 2 introduces problem  
 102 formulation and some necessary preliminaries. Section 3 provides the design  
 103 of local state observers to deal with unmeasured states and proposes an event-  
 104 trigger-based containment control strategy as well as stability analysis. Section  
 105 4 gives two simulation examples for verifying the effectiveness of the proposed  
 106 control strategy.

## 107 2 Problem Formulation and Preliminaries

### 108 2.1 System Dynamics

109 We consider a class of stochastic nonlinear MAS, the dynamic of the  $i$ th fol-  
 110 lower is given

$$\begin{cases} dx_{i,k} = (x_{i,k+1} + f_{i,k}(\bar{x}_{i,k})) dt + g_{i,k}^T(\bar{x}_i) dw_i, \\ dx_{i,n_i} = (u_i + f_{i,n_i}(\bar{x}_{i,n_i})) dt + g_{i,n_i}^T(\bar{x}_i) dw_i, \\ y_i = x_{i,1}, \end{cases} \quad (1)$$

111 where  $i = 1, \dots, N$ ,  $k = 1, \dots, n_i - 1$ ,  $n_i$  is the degree of the  $i$ th subsystem,  
 112  $\bar{x}_{i,j} = [x_{i,1}, \dots, x_{i,j}]^T \in \mathbb{R}^j$ ,  $j = 1, \dots, n_i$ ,  $\bar{x}_i = [x_{i,1}, \dots, x_{i,n_i}]^T \in \mathbb{R}^{n_i}$ , and

113  $\bar{x}_{i,j}$  denotes the state variables of the  $i$ th agent,  $u_i \in \mathbb{R}$  are the control inputs,  
 114  $y_i \in \mathbb{R}$  is the output of the  $i$ th agent,  $w_i$  represents the  $r$ -dimensional standard  
 115 Brownian motion defined on a complete probability space  $(\Omega, F, P)$  with  $\Omega$   
 116 being a sample space,  $F$  representing a  $\sigma$ -field, and  $P$  being a probability  
 117 measure.  $f_{i,j}(\cdot) : \mathbb{R}^j \rightarrow \mathbb{R}$  and  $g_{i,j}(\cdot) : \mathbb{R}^{n_i} \rightarrow \mathbb{R}^r$  are unknown, smooth and  
 118 bounded nonlinear functions.

119 **Definition 1** Consider a stochastic system

$$dx(t) = f[x(t)]dt + h^T[x(t)]dw. \quad (2)$$

120 For any given  $V(x) \in \mathbb{C}^2$ , the differential operator  $LV$  is defined as  $LV =$   
 121  $\frac{\partial V}{\partial t} + \frac{\partial V}{\partial x}f + \frac{1}{2}\text{Tr}\left\{h^T \frac{\partial^2 V}{\partial x^2} h\right\}$ , where  $\text{Tr}(A)$  represents the trace of the matrix  
 122  $A$ .

123 **Lemma 1** ([45, 46]) For the stochastic system (2), if there exists a contin-  
 124 uous differentiable Lyapunov function  $V$  such that

$$LV \leq -\alpha_0 V + \gamma_0, \quad (3)$$

125 where  $\alpha_0 > 0$  and  $\gamma_0 \geq 0$ , the system is bounded in probability.

126 **Lemma 2** ([47]) For  $\eta \in \mathbb{R}$  and constant  $t > 0$ , the inequality

$$0 \leq |\eta| - \eta \tanh\left(\frac{\eta}{t}\right) \leq \tau t \quad (4)$$

127 holds, where  $\tau = 0.2785$ .

## 128 2.2 Graph Theory

129 There are  $N$  followers, labeled as  $\nu_1$  to  $\nu_N$ , and  $M$  leaders, labeled as  $\nu_{N+1}$   
 130 to  $\nu_{N+M}$ .  $\mathcal{G} = (V_{\mathcal{G}}, \varepsilon_{\mathcal{G}})$  represents a communication topology of a directed  
 131 graph, where  $V_{\mathcal{G}} = \{\nu_1, \nu_2, \dots, \nu_{N+M}\}$  is denoted as a set of nodes, and  $\varepsilon_{\mathcal{G}} \subseteq$   
 132  $V_{\mathcal{G}} \times V_{\mathcal{G}}$  is a directed edge set.  $A_{ij} = (\nu_i, \nu_j) \in \varepsilon_{\mathcal{G}}$  represents agent  $j$  can obtain  
 133 information from  $i$ . The neighbors' set of  $\nu_i$  is defined as  $\mathcal{N}_i = \{\nu_j | A_{ji} \in \varepsilon_{\mathcal{G}}\}$ .  
 134 Communication topology of a digraph  $\mathcal{G}$  is represented by an adjacency matrix  
 135  $\mathcal{A} = [a_{ij}] \in \mathbb{R}^{(N+M) \times (N+M)}$ , if  $A_{ji} \in \varepsilon_{\mathcal{G}}$  is satisfied,  $a_{ij} > 0$ , otherwise  $a_{ij} = 0$ .  
 136 The value of  $a_{ij}$  denotes the communication weight from Agent  $j$  to Agent  
 137  $i$ . Laplacian matrix  $\ell$  of the directed graph  $\mathcal{G}$  is denoted by  $\ell = \mathcal{D} - \mathcal{A}$ ,  
 138  $\ell \in \mathbb{R}^{(N+M) \times (N+M)}$ , where  $\mathcal{D} = \text{diag}(d_1, \dots, d_{N+M})$  is the in-degree matrix  
 139 of Agent  $i$ , and  $d_i = \sum_{j=1}^{N+M} a_{ij}$  is the weighted in-degree. The matrix  $\ell$  can be  
 140 partitioned as

$$\ell = \begin{bmatrix} \bar{\ell}_1 & \bar{\ell}_2 \\ 0_{M \times N} & 0_{M \times M} \end{bmatrix} \quad (5)$$

141 where  $\bar{\ell}_1 \in \mathbb{R}^{N \times N}$  is a matrix related to the communication among  $N$  followers,  
 142 and  $\bar{\ell}_2 \in \mathbb{R}^{N \times M}$  denotes the communication relationship from  $M$  leaders to  
 143  $N$  followers.

144 **Definition 2** The set  $A \in \mathbb{R}^n$  is said to be convex if for any  $x_1, x_2 \in A$ ,  
 145  $\beta \in [0, 1]$ , and  $\beta x_1 + (1 - \beta)x_2$  is also in  $A$ . The convex envelope  $Co(X)$  for a  
 146 set of points  $X = \{x_1, x_2, \dots, x_n\}$  is defined as

$$Co(X) = \left\{ \sum_{i=1}^n \beta_i x_i \mid x_i \in X, \beta_i > 0, \sum_{i=1}^n \beta_i = 1 \right\}. \quad (6)$$

147 **Assumption 1** *There exists at least one leader that holds a directed path to*  
 148 *each follower.*

149 **Assumption 2** *The leaders' output signals  $y_{L,j} \in \mathbb{R}$  are smooth functions,*  
 150 *where  $y_{L,j}$  and  $\dot{y}_{L,j}$  are bounded and can be obtained by  $i$ th follower,  $j \in \mathcal{N}_i$ .*

151 **Lemma 3** ([48]) *Under Assumption 1, all eigenvalues of  $\bar{\ell}_1$  in (5) have pos-*  
 152 *itive real parts. Each entry of  $-\bar{\ell}_1^{-1}\bar{\ell}_2$  is nonnegative, and each row of  $-\bar{\ell}_1^{-1}\bar{\ell}_2$*   
 153 *has a sum equal to 1.*

154 The control objective is to design an event-trigger-based containment control  
 155 strategy  $u_i$  such that  $\inf_{h(t) \in Y_L(t)} E[\|y_i - h(t)\|] < \varepsilon, \forall \varepsilon > 0$ , where  $i =$   
 156  $1, 2, \dots, N$ ,  $Y_L(t) = Co\{y_{L,N+1}(t), \dots, y_{L,N+M}(t)\}$ , and all signals are bound-  
 157 ed in probability. Also, there exists Zeno-free behavior.

158 Denoting  $y_L = [y_{L,N+1}, \dots, y_{L,N+M}]^T$ , we obtain  $y_d = [y_{d,1}, \dots, y_{d,N}]^T =$   
 159  $-\bar{\ell}_1^{-1}\bar{\ell}_2 y_L$ . From Lemma 3, one has  $y_{d,i}(t) \in h(t)$ ,  $i = 1, \dots, N$ . Therefore,  
 160 the containment control problem is transformed into a tracking issue with one  
 161 leader  $\inf_{h(t) \in Y_L(t)} E[\|y_i - y_{d,i}\|] < \varepsilon$ , where  $i = 1, \dots, N$ . The containment errors  
 162 are defined as  $\rho_i = y_i - y_{d,i}$ . In vector,  $\rho = [\rho_1, \dots, \rho_N]^T$ ,  $y = [y_1, y_2, \dots, y_N]^T$ ,  
 163 and it follows  $\rho = y - y_d$ .

164 *Remark 1* In most existing results, an output signal from a controller is ap-  
 165 plied to the system often in a continuous manner [49, 50]. This manner is  
 166 scheduled regardless of whether system performance is necessary or not. It is  
 167 unreasonable as communication resources over a network are limited [51]. It  
 168 is a challenge to design a triggered mechanism for saving network resources.

169 *Remark 2* In most cases, system states are not able to measurable or even not  
 170 obtained directly [52]. As for unavailable information, it is hard to develop  
 171 control methods directly [53]. Thus, a local linear state observer is designed  
 172 to deal with the unmeasured states.

### 173 3 Observer-based Containment Output Control

174 An output feedback containment control strategy, including observer and out-  
 175 put controller, is presented.

176 3.1 Observer Design

177 A state observer is designed

$$\begin{cases} \dot{\hat{x}}_{i,k} = \hat{x}_{i,k+1} + l_{i,k}(y_i - \hat{x}_{i,1}), \\ \dot{\hat{x}}_{i,n_i} = u_i + l_{i,n_i}(y_i - \hat{x}_{i,1}), \end{cases} \quad (7)$$

178 where  $i = 1, \dots, N$ ,  $k = 1, \dots, n_i - 1$ ,  $\hat{x}_{i,j}$  is estimation of  $x_{i,j}$ , and  $l_{i,j}$  is a  
179 positive constant given later,  $j = 1, \dots, n_i$ .

180 The error vector of the observer is defined as

$$e_i = [e_{i,1}, e_{i,2}, \dots, e_{i,n_i}]^T = \bar{x}_i - \hat{x}_i, \quad (8)$$

181 where  $\hat{x}_i$  is the estimation of  $\bar{x}_i$ .

182 The derivative of  $e_i$ , according to (1), (7) and (8), is

$$de_i = (M_i e_i + f_i(\bar{x}_i))dt + \varphi_i^T(\bar{x}_i)dw_i, \quad (9)$$

183 where  $f_i(\bar{x}_i) = [f_{i,1}(\bar{x}_{i,1}), \dots, f_{i,n_i}(\bar{x}_{i,n_i})]^T$ ,  $M_i = \begin{bmatrix} -l_{i,1} & & & \\ -l_{i,2} & I_{n_i-1} & & \\ \vdots & & & \\ -l_{i,n_i} & 0 & \dots & 0 \end{bmatrix}$  is a  $n_i$ th-

184 order matrix,  $I_{n_i-1}$  is an identity matrix with  $(n_i - 1)$ th-order, and  $\varphi_i(\cdot)$  is  
185 the basis function vector. Due to the fact that  $M_i$  is a Hurwitz matrix, there  
186 exists a positive definite matrix  $K_i = K_i^T$  satisfying

$$M_i^T K_i + K_i M_i = -Q_i \quad (10)$$

187 for a positive matrix  $Q_i = Q_i^T$ .

188 *Remark 3* Indeed, not all choices of  $l_{i,j}$  would automatically result in  $M_i$  being  
189 Hurwitz, and we have to choose  $l_{i,j}$  appropriately such that the roots of a  
190 polynomial  $s^n + l_{i,1}s^{n-1} + \dots + l_{i,n_i-1}s + l_{i,n_i}$  have negative real parts.

191 Choose a Lyapunov function  $V_0 = \sum_{i=1}^N e_i^T K_i e_i$  for the observer. From (9)  
192 and (10), one has

$$LV_0 \leq \sum_{i=1}^N \left\{ -\lambda_{\min}(Q_i) \|e_i\|^2 + 2e_i^T K_i f_i(\bar{x}_i) \right\} + \sum_{i=1}^N \left\{ \text{Tr} \{ \varphi_i^T K_i \varphi_i \} \right\}, \quad (11)$$

193 where  $\lambda_{\min}(Q_i)$  is the minimum eigenvalue of  $Q_i$ .

194 From the Young's inequality and (11), we get

$$LV_0 \leq -\xi \|e_i\|^2 + \sum_{i=1}^N \left\{ \|K_i\|^2 \|\varepsilon_i\|^2 + \|K_i\|^2 W_i^* + \frac{1}{2} \|K_i\|^2 + \frac{1}{2} \|\varphi_i\|^2 \right\}, \quad (12)$$

195 where  $\varepsilon_i = [\varepsilon_{i,1}, \dots, \varepsilon_{i,n_i}]^T$ ,  $\xi = \min_{1 \leq i \leq N} \{\xi_i\}$  with  $\xi_i = \lambda_{\min}(Q_i) - 2$ , and  
 196  $W_i^* = \max \left\{ N_{i,k} \left\| \vartheta_{i,k}^* \right\|, k = 1, 2, \dots, n_i \right\}$  with  $N_{i,k} = \varphi_{i,k}^T \varphi_{i,k}$ .

197 From (12), we cannot obtain stability of the system, thus it is necessary  
 198 to design a suitable controller for the MAS, which will be discussed in the  
 199 following subsection.

### 200 3.2 Controller Design

201 With the observer in Section 3.1, we next make the following assumption for  
 202 controller design.

203 **Assumption 3** *The state  $\hat{x}_{j,2}$  of the  $j$ th follower is available for its neighbor*  
 204  *$j$  satisfying  $j \in \mathcal{N}_i$ .*

205 Define the error surfaces

$$z_{i,1} = \sum_{j=1}^N a_{ij}(y_i - y_j) + \sum_{j=N+1}^{N+M} a_{ij}(y_i - y_{L,j}), \quad (13)$$

206

$$z_{i,k} = \hat{x}_{i,k} - \pi_{i,k}, \quad (14)$$

207 where  $i = 1, \dots, N$ ,  $k = 2, \dots, n_i$ ,  $z_{i,1}$  is the distributed tracking error, and  
 208  $z_{i,k}$  is the error surface. Let the virtual control law  $\alpha_{i,k}$  pass through a first-  
 209 order filter

$$\sigma_{i,k+1} \dot{\pi}_{i,k+1} + \pi_{i,k+1} = \alpha_{i,k} \quad (15)$$

210 with  $\pi_{i,k+1}(0) = \alpha_{i,k}(0)$ , where  $i = 1, \dots, N$ ,  $k = 1, \dots, n_i - 1$ ,  $\sigma_{i,k+1}$  is a  
 211 positive constant, and  $\pi_{i,k}$  is the output of the first-order filter with virtual  
 212 control function as the input.

213 In order to eliminate the influence of error from the filter, the dynamic  
 214 equations of compensators are designed

$$\dot{\varpi}_{i,1} = -c_{i,1} \varpi_{i,1} + d_i \varpi_{i,2} + d_i (\pi_{i,2} - \alpha_{i,1}), \quad (16)$$

215

$$\dot{\varpi}_{i,k} = -c_{i,k} \varpi_{i,k} - \varpi_{i,k-1} + \varpi_{i,k+1} + \pi_{i,k+1} - \alpha_{i,k}, \quad (17)$$

216

$$\dot{\varpi}_{i,n_i} = -c_{i,n_i} \varpi_{i,n_i} - \varpi_{i,n_i-1}, \quad (18)$$

217 where  $c_{i,1}$ ,  $c_{i,k}$  and  $c_{i,n_i}$  are positive constants,  $\varpi_{i,1}(0) = 0$ ,  $\varpi_{i,k}(0) = 0$  and  
 218  $\varpi_{i,n_i}(0) = 0$ ,  $k = 2, \dots, n_i - 1$ , and  $\alpha_{i,k}$  are virtual control laws designed in  
 219 the following paper. The term for compensation of tracking error is defined as

$$v_{i,k} = z_{i,k} - \varpi_{i,k}, \quad i = 1, \dots, N, \quad k = 1, \dots, n_i. \quad (19)$$

Radial basis function NNs are for approximation of  $\bar{f}_{i,k}(\bar{Z}_{i,k}) = \vartheta_{i,k}^{*T} \varphi_{i,k}(\bar{Z}_{i,k}) + \delta_{i,k}(\bar{Z}_{i,k})$ , where  $\bar{Z}_{i,k} = [\hat{x}_{j,2}, x_{i,1}, \hat{x}_{i,1}, v_{i,k}, \hat{y}_{L,j}]^T$ ,  $j \in \mathcal{N}_i$ ,  $i = 1, \dots, N$ ,  $k = 1, \dots, n_i$ .  $\vartheta_{i,k}^*$  is the ideal constant weight vector defined by

$$\vartheta^* = \arg \min_{\vartheta \in \mathbb{R}^l} \left\{ \sup_{Z \in \Omega_Z} |f(Z) - \vartheta^T \varphi(Z)| \right\},$$

with  $l > 1$  denoting the neural network number and  $\delta$  being the minimum approximation error.

The virtual control laws are designed as

$$\alpha_{i,1} = -\frac{c_{i,1}}{d_i} z_{i,1} - \frac{1}{2r_{i,1}} \hat{W}_i v_{i,1}, \quad (20)$$

$$\alpha_{i,k} = -c_{i,k} z_{i,k} - z_{i,k-1} - \frac{1}{2r_{i,k}} \hat{W}_i v_{i,k} + \dot{\pi}_{i,k}, \quad (21)$$

with adaptive laws

$$\dot{\hat{W}}_i = \frac{\gamma_i}{2r_{i,1}} d_i v_{i,1}^2 + \sum_{k=2}^{n_i} \frac{\gamma_i}{2r_{i,k}} v_{i,k}^2 - \gamma_i \lambda_i \hat{W}_i, \quad (22)$$

where  $i = 1, 2, \dots, N$ ,  $k = 2, \dots, n_i$ ,  $N_{i,k} = \phi_{i,k}^T \phi_{i,k}$ ,  $r_{i,1}$ ,  $r_{i,k}$ ,  $\gamma_i$  and  $\lambda_i$  are positive design parameters,  $W_i^* = \max \left\{ N_{i,k} \|\vartheta_{i,k}^*\|^2, k = 1, 2, \dots, n_i \right\}$ , and  $\hat{W}_i$  is estimation of  $W_i^*$ .

The control strategy based on fixed threshold

$$u_i(t) = \chi_i(t_p), \forall t \in [t_p, t_{p+1}) \quad (23)$$

is presented with

$$\chi_i(t) = \alpha_{i,n_i} - \bar{m}_i \tanh \left( \frac{\nu_{i,n_i} \bar{m}_i}{\varepsilon_i} \right) \quad (24)$$

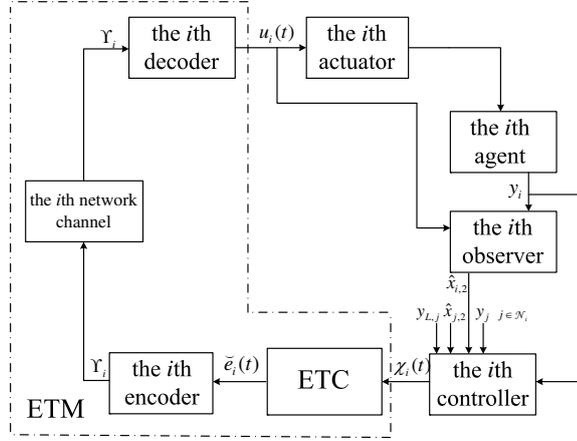
and the following event-triggered mechanism

$$t_{i,p+1} = \inf \{ t > t_{i,p} \mid |\check{e}_i(t)| \geq m_i \}, t_{i,0} = 0, \quad (25)$$

where  $\check{e}_i(t) = \chi_i(t) - u_i(t)$  represents the error caused by the event-triggered mechanism (ETM),  $\varepsilon_i$ ,  $m_i$  and  $\bar{m}_i$  are design positive parameters,  $\bar{m}_i > m_i$ ,  $t_{i,p}$  is the triggered instant,  $t_{i,p+1}$  is determined by (25), and  $\chi_i(t_{i,p})$  holds as a constant during triggered interval  $t \in [t_{i,p}, t_{i,p+1})$ .

A diagram for control signal transmission is presented in Fig. 1. The initial value  $u_i(t_{i,0})$  is transmitted through a network channel after encoding. For  $t \in [t_{i,p}, t_{i,p+1})$ ,  $p = 1, 2, \dots$ , the triggered condition,  $|\check{e}_i(t)| \geq m_i$ , is checked. Then the digital signal 0/1 will be transmitted according to the event-triggered condition (ETC). The output of the encoder is transmitted to the decoder

240 through the network channel. And the control signal changes on the basis of  
 241 the digital signal received from the decoder accordingly.



**Fig. 1** A diagram for control signal transmission.

242 *Remark 4* In this paper, the DSC method is used to design the control law. If  
 243 the traditional backstepping method is used, the following derivation can be  
 244 obtained.

245 Step  $i, 1$ : Taking the derivative of (13) and with (7), we have

$$\begin{aligned} dz_{i,1} = & \left( d_i (\hat{x}_{i,2} + e_{i,2} + f_{i,1}) - \sum_{j=N+1}^{N+M} a_{ij} \dot{y}_{L,j} - \sum_{j=1}^N a_{ij} (\hat{x}_{j,2} + e_{j,2} + f_{j,1}) \right) dt \\ & + d_i g_{i,1}^T dw_i + \sum_{j=1}^N a_{ij} g_{i,1}^T dw_j. \end{aligned} \quad (26)$$

246 Step  $i, 2$ : Define the error surface

$$z_{i,2} = \hat{x}_{i,2} - \alpha_{i,1}, \quad (27)$$

247 and its derivative is

$$dz_{i,2} = d\hat{x}_{i,2} - d\alpha_{i,1}. \quad (28)$$

248 Then, we can get

$$d\alpha_{i,1} = \check{\eta}_{i,1} dt + g_{i,1}^T \frac{\partial \alpha_{i,1}}{\partial \hat{x}_{i,1}} dw_i, \quad (29)$$

249 where  $\check{\eta}_{i,1} = \sum_{j=N+1}^{N+M} \frac{\partial \alpha_{i,1}}{\partial y_{L,j}} \dot{y}_{L,j} + \frac{\partial \alpha_{i,1}}{\partial \dot{W}_1} \dot{W}_1 + \frac{1}{2} g_{i,1}^T g_{i,1} \frac{\partial^2 \alpha_{i,1}}{\partial \hat{x}_{i,1}^2} + \frac{\partial \alpha_{i,1}}{\partial \hat{x}_{i,1}} (x_{i,2} + f_{i,1})$ .

250 Thus, one has

$$dz_{i,2} = \left( \check{\eta}_{i,1} + \hat{x}_{i,3} + l_{i,2}(y_i - \hat{x}_{i,1}) \right) dt + g_{i,1}^T \frac{\partial \alpha_{i,1}}{\partial \hat{x}_{i,1}} dw_i. \quad (30)$$

251 From (26) and (30), we can see that the traditional backstepping control  
 252 approach essentially suffers from the main problem as explosion of complexity  
 253 owing to repeated differentiations of virtual controllers. The strategy in our  
 254 paper uses simple algebraic operation instead of complex derivation process.  
 255 It introduces a first-order filtering of the virtual control law at each step of the  
 256 backstepping design procedure. Also, a compensator is designed to eliminate  
 257 the effect from a filter in containment control.

### 258 3.3 Stability analysis

259 **Theorem 1** *The stochastic MAS is composed of  $M$  leaders and  $N$  followers.*  
 260 *Under Assumption 1–Assumption 3, the event-triggered control strategy (23)*  
 261 *with the state observer (8) and adaptive law (22) ensures the output of fol-*  
 262 *lowers is in a convex hull formed by the leaders' trajectories. The containment*  
 263 *error converges to the neighborhood around the origin in probability with ap-*  
 264 *propriate parameters. All signals in the MAS are bounded in probability, and*  
 265 *there exists Zeno-free behavior.*

266 *Proof* From (13) and (19), we obtain

$$\begin{aligned} v_{i,1} &= z_{i,1} - \varpi_{i,1} \\ &= \sum_{j=1}^N a_{ij}(y_i - y_j) + \sum_{j=N+1}^{N+M} a_{ij}(y_i - y_{L,j}) - \varpi_{i,1}. \end{aligned} \quad (31)$$

267 With (1), the derivative of (31) is

$$\begin{aligned} dv_{i,1} &= \left( d_i(v_{i,2} + e_{i,2} + \alpha_{i,1} + f_{i,1}) + c_{i,1}\varpi_{i,1} - \sum_{j=1}^N a_{ij}(\hat{x}_{j,2} + e_{j,2} + f_{j,1}) - \sum_{j=N+1}^{N+M} a_{ij}\dot{y}_{L,j} \right) dt \\ &\quad + d_i g_{i,1}^T dw_i - \sum_{j=1}^N a_{ij} g_{i,1}^T dw_j, \end{aligned}$$

268 where  $i = 1, \dots, N$ .

269 For the first subsystem, the Lyapunov function is selected as

$$V_{i,1} = \frac{1}{2} v_{i,1}^2. \quad (32)$$

270 With (32) and Definition 1, one has

$$LV_{i,1} \leq v_{i,1} \left( d_i(v_{i,2} + e_{i,2} + \alpha_{i,1} + \bar{f}_{i,1}(\bar{Z}_{i,1}) - v_{i,1}) - \frac{1}{2}v_{i,1} \sum_{j=1}^N a_{ij} - \sum_{j=1}^N a_{ij}e_{j,2} + c_{i,1}\varpi_{i,1} \right) \\ + \frac{1}{2}d_i^2 g_{i,1}^T g_{i,1} + \frac{1}{2} \sum_{j=1}^N a_{ij} g_{j,1}^T \sum_{j=1}^N a_{ij} g_{j,1},$$

271 where  $\bar{f}_{i,1}(\bar{Z}_{i,1}) = f_{i,1} + v_{i,1} + \frac{1}{2d_i} \sum_{j=1}^N a_{ij}v_{i,1} - \frac{1}{d_i} \sum_{j=1}^N a_{ij}(\hat{x}_{j,2} + f_{j,1}) -$   
272  $\frac{1}{d_i} \sum_{j=N+1}^{N+M} a_{ij}\dot{y}_{L,j}$ . From Young's inequality, the equation can be rewritten as

$$LV_{i,1} \leq v_{i,1} \left( d_i(v_{i,2} + \alpha_{i,1} + \bar{f}_{i,1}(\bar{Z}_{i,1}) - \frac{1}{2}v_{i,1}) + c_{i,1}\varpi_{i,1} \right) \quad (33)$$

$$+ \frac{1}{2}d_i\|e_i\|^2 + \frac{1}{2}\|e_i\|^2 \sum_{j=1}^N a_{ij} + \frac{1}{2}d_i^2 g_{i,1}^T g_{i,1} + \frac{N}{2} \sum_{j=1}^N a_{ij}^2 g_{j,1}^T g_{j,1}. \quad (34)$$

273 For the  $k$ th subsystem,  $k = 2, \dots, n_i - 1$ , along with (14) and (19), one  
274 has

$$v_{i,k} = z_{i,k} - \varpi_{i,k} = \hat{x}_{i,k} - \pi_{i,k} - \varpi_{i,k}. \quad (35)$$

275 Choose a Lyapunov function  $V_{i,k} = \frac{1}{2}v_{i,k}^2$ . From the observer (7) and (35), we  
276 have

$$LV_{i,k} \leq v_{i,k} \left( v_{i,k+1} + \alpha_{i,k} + \bar{f}_{i,k}(\bar{Z}_{i,k}) - \frac{1}{2}v_{i,k} + c_{i,k}\varpi_{i,k} + \varpi_{i,k-1} - \dot{\pi}_{i,k} \right), \quad (36)$$

277 where  $\bar{f}_{i,k}(\bar{Z}_{i,k}) = l_{i,k}(y_i - \hat{x}_{i,1}) + \frac{1}{2}v_{i,k}$ , and  $l_{i,k}$  is a positive constant.

278 Finally, for the  $n_i$ th subsystem, one has  $v_{i,n_i} = z_{i,n_i} - \varpi_{i,n_i} = \hat{x}_{i,n_i} -$   
279  $\pi_{i,n_i} - \varpi_{i,n_i}$ , and select a Lyapunov function

$$V_{i,n_i} = \frac{1}{2}v_{i,n_i}^2. \quad (37)$$

280 Within the event-triggered interval  $t \in [t_k, t_{k+1})$ , one has  $|\chi_i(t) - u_i(t)| \leq$   
281  $m_i$  from (25). There exists a time-varying parameter  $\lambda_i$  such that  $\lambda_i(t_k) =$   
282  $0$ ,  $\lambda_i(t_{k+1}) = \pm 1$ ,  $|\lambda_i(t)| \leq 1$ . Then,  $\forall t \in [t_k, t_{k+1})$ , we rewrite the control  
283 strategy

$$\chi_i(t) = u_i(t) + \lambda_i(t)m_i. \quad (38)$$

284 With (7), (14), (24), (37), (38), and Lemma 2, we further get

$$LV_{i,n_i} \leq v_{i,n_i} \left( \alpha_{i,n_i} + \bar{f}_{i,n_i}(\bar{Z}_{i,n_i}) - \frac{1}{2}v_{i,n_i} + c_{i,n_i}\varpi_{i,n_i} + \varpi_{i,n_i-1} - \dot{\pi}_{i,n_i} \right), \quad (39)$$

285 where  $\bar{f}_{i,n_i}(\bar{Z}_{i,n_i}) = l_{i,n_i}(y_i - \hat{x}_{i,1}) + \frac{1}{2}v_{i,n_i} + 0.2785\epsilon_i$ .

286 We choose the following Lyapunov function  $V = V_0 + \sum_{i=1}^N \left\{ V_{i,0} + \frac{1}{2\gamma_i} \tilde{W}_i^2 \right\}$ ,  
 287 where  $V_{i,0} = \frac{1}{2} \sum_{k=1}^{n_i} V_{i,k}$ , and  $\tilde{W}_i = W_i^* - \hat{W}_i$ . Then, with (34), (36), (39),  
 288  $0.5d_i + 0.5 + c_i \leq c_{i,1}$ ,  $0.5d_i + 1.5 + c_i \leq c_{i,2}$ ,  $2 + c_i \leq c_{i,k}$ ,  $k = 3, \dots, n_i - 1$ ,  $1 +$   
 289  $c_i \leq c_{i,n_i}$ , where  $c_i > 0$ ,  $i = 1, \dots, N$ , and Young's inequality  $v_{i,k} \tilde{f}_{i,k}(Z_{i,k}) \leq$   
 290  $\frac{1}{2}v_{i,k}^2 + \frac{1}{2r_{i,k}}v_{i,k}^2 W_i^* + \frac{1}{2}r_{i,k} + \frac{1}{2}\varepsilon_{i,k}^2$ , one has

$$\begin{aligned} LV \leq & - \left[ \xi - \frac{1}{2} \sum_{i=1}^N a_{ij} - \frac{1}{2} \sum_{i=1}^N d_i \right] \|e_i\|^2 + \sum_{i=1}^N \left[ - \sum_{k=1}^{n_i} c_i v_{i,k}^2 - \frac{1}{2} \lambda_i \tilde{W}_i^2 + \frac{1}{2} d_i r_{i,1} \right. \\ & + \frac{1}{2} \sum_{k=2}^{n_i} r_{i,k} + \frac{1}{2} d_i \varepsilon_{i,1}^2 + \frac{1}{2} \sum_{k=2}^{n_i} \varepsilon_{i,k}^2 + \|K_i\|^2 \|\varepsilon_i\|^2 + \|K_i\|^2 W_i^* + \frac{1}{2} \|K_i\|^2 \\ & \left. + \frac{1}{2} d_i^2 g_{i,1}^T g_{i,1} + \frac{N}{2} \sum_{j=1}^N a_{ij}^2 g_{j,1}^T g_{j,1} + \frac{1}{2} |g_{i,1}^T g_{i,1}|^2 + \frac{1}{2} \lambda_i W_i^{*2} \right], \end{aligned}$$

291 where  $c_i$  is a design parameter. (40) can be rewritten as

$$LV \leq -Q_1 V + Q_2, \quad (40)$$

292 where  $Q_1 = \min \left\{ \xi - \frac{1}{2} \sum_{i=1}^N (a_{ij} + d_i), \min\{2c_i\}, \min\{\gamma_j \lambda_j\} \right\}$ ,  $i = 1, \dots, N$ ,  $j =$   
 293  $1, \dots, n_i$ ,  $Q_2 = \sum_{i=1}^N \left\{ \frac{1}{2} d_i \varepsilon_{i,1}^2 + \frac{1}{2} \sum_{k=2}^{n_i} \varepsilon_{i,k}^2 + \|K_i\|^2 \|\varepsilon_i\|^2 + \|K_i\|^2 W_i^* + \frac{1}{2} \|K_i\|^2 + \right.$   
 294  $\left. \frac{1}{2} d_i r_{i,1} + \frac{1}{2} \sum_{k=2}^{n_i} r_{i,k} + \frac{1}{2} d_i^2 g_{i,1}^T g_{i,1} + \frac{N}{2} \sum_{j=1}^N a_{ij}^2 g_{j,1}^T g_{j,1} + \frac{1}{2} |g_{i,1}^T g_{i,1}|^2 + \frac{1}{2} \lambda_i W_i^{*2} \right\}$ .

295 Now, we prove that the Zeno behavior will be avoided, i.e., time interval  
 296  $t^* > 0$  between any two trigger events that satisfies  $\forall k \in z^+$ ,  $t_{k+1} - t_k \geq t^*$ .

297 From  $e_i(t) = \chi_i(t) - u_i(t)$ ,  $\forall t \in [t_k, t_{k+1})$ , the time derivative of the  
 298 trigger errors  $e_i$  is given,  $\frac{d}{dt} |e_i| = \frac{d}{dt} (e_i * e_i)^{\frac{1}{2}} = \text{sign}(e_i) \dot{e}_i \leq |\dot{\chi}_i|$ . From (24),

299  $\dot{\chi}_i$  is obtained  $\dot{\chi}_i(t) = \dot{\alpha}_{i,n_i} - \frac{\bar{m}_i^2 v_{i,n_i}}{\varepsilon_i \cosh^2\left(\frac{\bar{m}_i v_{i,n_i}}{\varepsilon_i}\right)}$ . Due to the fact that  $f_i(\cdot)$  is

300 continuously differentiable,  $\dot{\chi}_i$  is a continuous function.  $x_i$  are global bounded,  
 301 and there exists a constant  $\kappa > 0$ , such that  $|\dot{\chi}_i| \leq \kappa$ . From  $e_i(t_k) = 0$  and  
 302  $\lim_{t \rightarrow t_{k+1}^-} e_i(t) = m$ , we can find a constant  $t^*$  satisfying  $t^* \geq \frac{m}{\kappa}$ ,  $t_{k+1} - t_k \geq t^*$ .

303 Thus, there exists Zeno-free behavior.

304 Integrating equation (40) yields

$$0 \leq EV(t) \leq \frac{Q_2}{Q_1} (1 - \exp(-Q_1 t)) + EV(x(0), 0). \quad (41)$$

305 Then, one has

$$EV(t) \leq \frac{Q_2}{Q_1}, \forall t > T_1, \quad (42)$$

306 where  $T_1 = \max \left\{ 0, \frac{1}{Q_1} \ln \left( \frac{Q_1}{Q_2} \text{EV}(0) \right) \right\}$ . Then, from (42), the bounds of errors  
 307 in the close-loop system are obtained

$$\sum_{i=1}^N \sum_{k=1}^{n_i} \mathbb{E} \left[ |v_{i,k}|^2 \right] \leq 2 \frac{Q_2}{Q_1}, \forall t > T_1, \quad (43)$$

308

$$\sum_{i=1}^N \frac{1}{\gamma_i} \mathbb{E} \left[ |\tilde{W}_i|^2 \right] \leq 2 \frac{Q_2}{Q_1}, \forall t > T_1, \quad (44)$$

309 and

$$\sum_{i=1}^N \lambda_{\min}(K_i) \mathbb{E} \left[ \|e_i\|^2 \right] \leq \frac{Q_2}{Q_1}, \forall t > T_1. \quad (45)$$

310 The compensation signal  $\varpi_i$  eventually converges to a compact set  $\phi_{\bar{\omega}_{i,1}} =$   
 311  $\left\{ \bar{\omega}_{i,1} = [|\bar{\omega}_{i,1}|, \dots, |\bar{\omega}_{i,n_i}|]^T \in \mathbb{R}^N \mid \|\bar{\omega}_{i,1}\| \leq \sum_{i=1}^N \frac{\xi_i}{\sigma_i} \right\}$ , where  $|\pi_{i,k+1} - \alpha_{i,k}| \leq$   
 312  $\xi_i$ , and  $\sigma_i = \min(c_{i,k})$ . From (43), it can be seen that  $v_{i,1}$  is bounded, and the  
 313 bound of the error  $z_{i,1}$  is  $\phi_{\bar{z}_{i,1}} = \left\{ \bar{z}_{i,1} = [|\bar{z}_{i,1}|, \dots, |\bar{z}_{i,n_i}|]^T \in \mathbb{R}^N \mid \|\bar{z}_{i,1}\| \leq \right.$   
 314  $\left. \sum_{i=1}^N \frac{\xi_i}{\sigma_i} + \sqrt{\frac{Q_2}{Q_1}}, \forall t > T_1 \right\}$ . From  $\bar{z}_1 = \bar{\ell}_1 y + \bar{\ell}_2 y_L$ , one has  $\lim_{t \rightarrow \infty} \|y + \bar{\ell}_1^{-1} \bar{\ell}_2 y_L\| \leq$   
 315  $\frac{\|\bar{z}_1\|}{\|\bar{\ell}_1\|_F}$ . With  $y_d = -\bar{\ell}_1^{-1} \bar{\ell}_2 y_L$ , the containment error satisfies  $\|\rho\| = \|y - y_d\| \leq$   
 316  $\frac{\|\bar{z}_1\|}{\|\bar{\ell}_1\|_F}$ . Thus, as  $t > T_1$ , it reveals that

$$\phi_\rho = \left\{ \rho \in \mathbb{R}^N \mid \mathbb{E} [\|\rho\|] \leq \sum_{i=1}^N \frac{\xi_i}{\|\bar{\ell}_1\|_F \sigma_i} + \frac{1}{\|\bar{\ell}_1\|_F} \sqrt{\frac{Q_2}{Q_1}} \leq \delta \right\}. \quad (46)$$

317 The proof is completed.

318 *Remark 5* In (10), the eigenvalues of the matrices  $K_i$ ,  $Q_i$  and  $M_i^T M_i$  are  
 319 recorded as  $0 \leq \check{\alpha}_1 \leq \check{\alpha}_2 \leq \dots \leq \check{\alpha}_n$ ,  $0 \leq \check{\beta}_1 \leq \check{\beta}_2 \leq \dots \leq \check{\beta}_n$ , and  
 320  $0 \leq \check{\sigma}_1 \leq \check{\sigma}_2 \leq \dots \leq \check{\sigma}_n$ , respectively. Here,  $\check{\alpha}_1 \geq \frac{\check{\beta}_1}{2\sqrt{\check{\sigma}_n}}$  and  $\check{\alpha}_n \geq \frac{\check{\beta}_n}{2\sqrt{\check{\sigma}_n}}$  hold.

321 As  $\check{\sigma}_n$  increases and  $\check{\beta}_1, \check{\beta}_n$  remains unchanged, the bounds of the maximum  
 322 and minimum eigenvalues of  $K_i$  decrease. Accordingly, the value of  $Q_2$  tends  
 323 to small resulting small size of the compact of the containment error.

324 *Remark 6* To show the advantage of the proposed strategy, we calculate the  
 325 bound of containment error via traditional DSC approach.  $\mathbb{E} [\|\rho\|] \leq \sum_{i=1}^N \frac{\xi_i}{\|\bar{\ell}_1\|_F \sigma_i} +$   
 326  $\frac{1}{\|\bar{\ell}_1\|_F} \sqrt{\frac{Q_2 + C}{Q_1}}$ . A term  $C = \frac{1}{2} \|z_{i,1}\|^2 \|s_{i,1}\|^2 + \frac{1}{2} \sum_{k=2}^{n_i-1} \|z_{i,k}\|^2 \|s_{i,k}\|^2$  is addi-  
 327 tional from filter errors in the traditional DSC, and it is not zero in most cases.  
 328 In our paper, the bound of containment error converges to a smaller size of

compact set without the additional term due to the compensator. Compensating signals leads to a small size of the compact set for closed-loop errors in an MAS. The advantage of this command filter is generating command signals to remove the influence from error vectors. In this manner, it indicates that the containment performance is improved in our paper.

## 4 Simulation Example

### 4.1 A Team of Robots

The dynamics of each robot are

$$\begin{cases} M_i \ddot{x}_i + B_{x_i} \dot{x}_i = f_{x_i} - k_{x_{d_i}} \dot{x}_i, \\ M_i \ddot{y}_i + B_{y_i} \dot{y}_i = f_{y_i} - k_{y_{d_i}} \dot{y}_i, \end{cases} \quad (47)$$

where  $M_i$  is the mass of a robot,  $B_{x_i}$  and  $B_{y_i}$  represent damper coefficients, and  $k_{x_{d_i}}$  and  $k_{y_{d_i}}$  are coefficients controlling the transient response.

Let  $x_{i,1,1} = x_i$ ,  $x_{i,1,2} = \dot{x}_i$ ,  $u_{i,1} = u_{x_i}$ ,  $x_{i,2,1} = y_i$ ,  $x_{i,2,2} = \dot{y}_i$ , and  $u_{i,2} = u_{y_i}$ . (47) is rewritten as

$$\begin{cases} dx_{i,1,1} = f_{i,1,1}(x_{i,1,1}, x_{i,1,2})dt + \sigma_{i,1,1}x_{i,1,1}dw_i, \\ dx_{i,1,2} = f_{i,1,2}(\bar{x}_{i,1,2}, u_{i,1})dt + \sigma_{i,1,2}x_{i,1,2}dw_i, \\ dx_{i,2,1} = f_{i,2,1}(x_{i,2,1}, x_{i,2,2})dt + \sigma_{i,2,1}x_{i,2,1}dw_i, \\ dx_{i,2,2} = f_{i,2,2}(\bar{x}_{i,2,2}, u_{i,2})dt + \sigma_{i,2,2}x_{i,2,2}dw_i, \\ y_{i,1} = x_{i,1,1}, \\ y_{i,2} = x_{i,2,1}, \end{cases} \quad (48)$$

where  $\sigma_{i,1,1}, \sigma_{i,1,2}, \sigma_{i,2,1}, \sigma_{i,2,2}$  are design parameters,  $y_{i,1}, y_{i,2}$  are coordinates of the followers,  $\bar{x}_{i,1,2} = [x_{i,1,1}, x_{i,1,2}]^T$ ,  $\bar{x}_{i,2,2} = [x_{i,2,1}, x_{i,2,2}]^T$ ,  $u_{i,1}$  and  $u_{i,2}$  are control inputs,

$$\begin{cases} f_{i,1,1}(x_{i,1,1}, x_{i,1,2}) = x_{i,1,2}, \\ f_{i,1,2}(\bar{x}_{i,1,2}, u_{i,1}) = [-(B_{x_i} + k_{x_{d_i}})x_{i,1,2} + u_{i,1}]/M_i, \\ f_{i,2,1}(x_{i,2,1}, x_{i,2,2}) = x_{i,2,2}, \\ f_{i,2,2}(\bar{x}_{i,2,2}, u_{i,2}) = [-(B_{y_i} + k_{y_{d_i}})y_{i,1,2} + u_{i,2}]/M_i, \end{cases} \quad (49)$$

$i = 1, 2, 3$ ,  $M_i = 1$ ,  $B_{x_i} = B_{y_i} = 1$ , and  $k_{x_{d_i}} = k_{y_{d_i}} = 9$ .

The leaders' trajectories are chosen as  $y_{L,4} = [t, \sin(t/2)]^T$ ,  $y_{L,5} = [0.8t - 0.5, \sin(t/2)]^T$ ,  $y_{L,6} = [0.8t - 0.5, \sin(t/3) - 0.5]^T$ ,  $y_{L,7} = [t, \sin(t/3) - 0.5]^T$ . Initial states are  $x_{1,1}(0) = [0.1, 0]^T$ ,  $x_{2,1}(0) = [0.1, 0]^T$ ,  $x_{3,1}(0) = [0.1, 0]^T$ ,  $x_{1,2}(0) = [0.2, 0]^T$ ,  $x_{2,2}(0) = [0.05, 0]^T$ ,  $x_{3,2}(0) = [0.3, 0]^T$ . The triggered threshold of each agent is 0.5. The parameters of the first-order filter, observer, adaptive law and control law are selected as  $l_{i,1,1} = l_{i,2,1} = 10$ ,  $l_{i,1,2} = l_{i,2,2} = 150$ ,  $\sigma_{i,1,2} = \sigma_{i,2,2} = 0.1$ ,  $c_{1,1,1} = 10$ ,  $c_{1,1,2} = c_{2,1,2} = c_{1,2,2} = c_{3,2,2} = 5$ ,  $c_{2,1,1} = c_{1,2,1} = c_{3,2,1} = 15$ ,  $c_{3,1,1} = 20$ ,  $c_{3,1,2} = 25$ ,  $c_{2,2,1} = 45$ ,  $c_{2,2,2} = 35$ ,  $r_{i,1} = r_{i,2} = 15$ ,  $\gamma_{i,1} = \gamma_{i,2} = 1$ ,  $\lambda_i = 1$ , where  $i = 1, 2, 3$ .

354 The directed network topology for the MAS is shown in Fig.2, and the sim-  
 355 ulation results are shown in Fig.2–Fig.7. Table.1 records the followers’ event-  
 356 triggered number in the Y-axis direction. It can be seen that, with the event-  
 357 triggered mechanism, the triggered number is much less than that without  
 358 time-triggered one. The containment performance is shown in Fig.3, and, at  
 359 three different times  $t = 4s, 12s, 25s$ , it can be seen that the output of the  
 360 followers can be well maintained in the convex hull formed by the leaders.  
 361 Fig.4 and Fig.5 show the event-triggered instants of three agents at X- and  
 362 Y-axis directions respectively. In Fig.6 and Fig.7, the adaptive parameters of  
 363 three followers are presented, respectively.

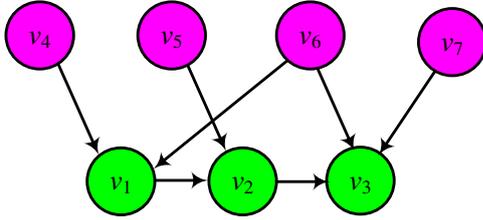
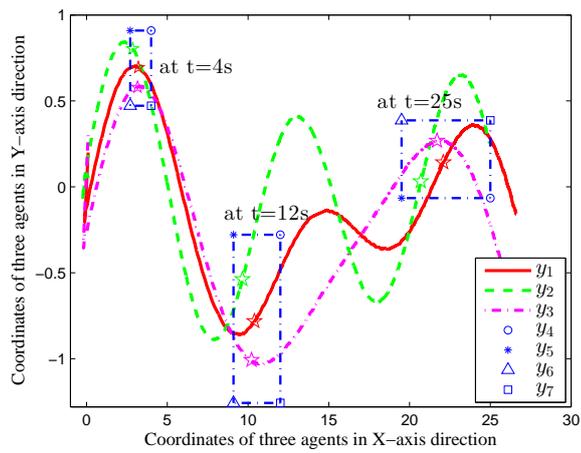


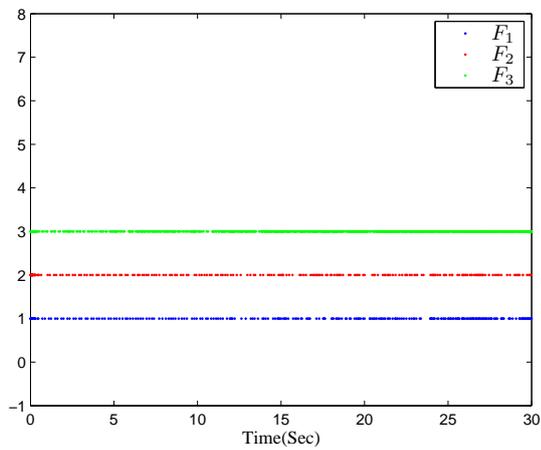
Fig. 2 Communication topology in Example A.

Table 1 Comparison of triggered number in Y-axis direction.

Strategy	Follower	Triggered Number
Event-triggered Strategy	1	215
	2	549
	3	255
Time-triggered Strategy	1&2&3	30005



**Fig. 3** Outputs of the three followers and the containment range at different instants  $t = 4s, 12s, 25s$ .



**Fig. 4** Triggered instant at X-axis direction.

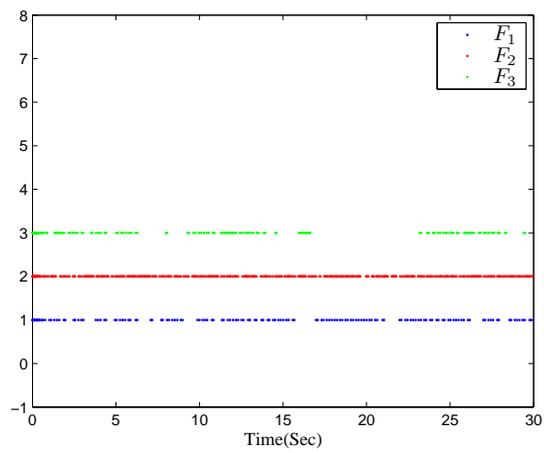


Fig. 5 Triggered instant at Y-axis direction.

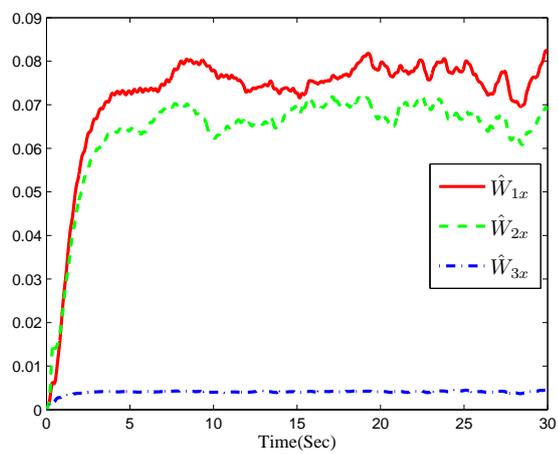
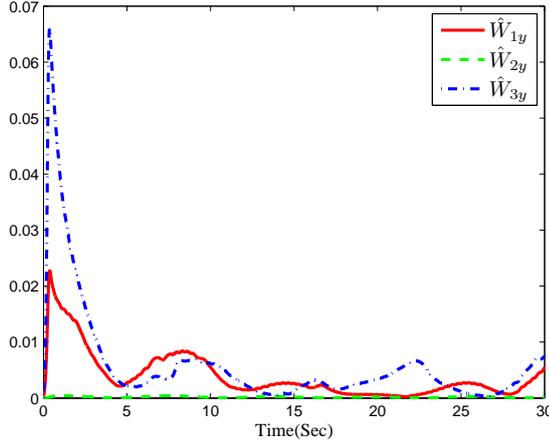


Fig. 6 The adaptive law at X-axis direction.



**Fig. 7** The adaptive law at Y-axis direction.

#### 364 4.2 A Numerical Example

365 Consider the following dynamics of the  $i$ th follower

$$\begin{cases} dx_{i,1} = (x_{i,2} + x_{i,1}(1 - \sin(x_{i,1}))^2)dt + 0.5 \cos(x_{i,1})dw_i, \\ dx_{i,2} = (u_i - 3.5x_{i,2} + x_{i,1}x_{i,2}^2)dt + 0.1x_{i,1} \sin(2x_{i,1}x_{i,2})dw_i, \\ y_i = x_{i,1}, \end{cases} \quad (50)$$

366 where  $i = 1, 2, 3, 4$ ,  $x_{i,1}, x_{i,2}$  are state variables, and  $y_i$  is follower's output. A  
 367 communication topology is shown in Fig.8. Two leaders' outputs are selected as  
 368  $y_{L,4} = \sin(t)$ ,  $y_{L,5} = 0.2(\sin(t) + \sin(0.5t))$ . Parameters are chosen as  $l_{i,1} = 10$ ,  
 369  $l_{i,2} = 150$ ,  $\sigma_{i,2} = 0.1$ ,  $c_{1,1} = 35$ ,  $c_{1,2} = c_{22} = 25$ ,  $c_{21} = 45$ ,  $c_{31} = 20$ ,  $c_{32} = 35$ ,  
 370  $r_{i,1} = r_{i,2} = 15$ ,  $\gamma_{i,1} = \gamma_{i,2} = 1$ ,  $\lambda_i = 1$ , where  $i = 1, 2, 3, 4$ .

371 The simulation results are given in Fig.9–Fig.21. The red and orange lines  
 372 in Fig.9 represent the outputs of the two leaders, respectively. It indicates  
 373 that the control strategy governs the MAS with satisfied performance. It can  
 374 be seen that the observers work well from Fig.11–Fig.13. Fig.14 represents  
 375 the adaptive laws of three agents. Fig.15 shows the event-triggered instant  
 376 of three agents. In Fig.16–Fig.18, the relationship between the trigger error  
 377 and the threshold values is given, and the triggered thresholds are 0.2, 0.8  
 378 and 1.2, respectively. The bar chart shows the corresponding number of event-  
 379 triggered in Fig.19. It can be concluded that, as the threshold scales down,  
 380 this mechanism results in more triggered number. Fig.20 is the comparison of  
 381 containment error with or without compensation signal. It can be seen that  
 382 the containment error of the follower with compensator is smaller than the  
 383 value without compensation signal. Table.2 lists three cases of parameters  $c_{1,1}$   
 384 and  $c_{1,2}$ , and Fig.21 shows the comparison of containment error in the three  
 385 cases. With the increase of parameters  $c_{1,1}$  and  $c_{1,2}$ ,  $Q_1$  in (46), the size of the  
 386 compact of the containment error becomes smaller.

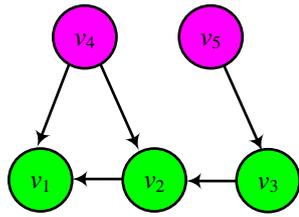


Fig. 8 Communication topology in Example B.

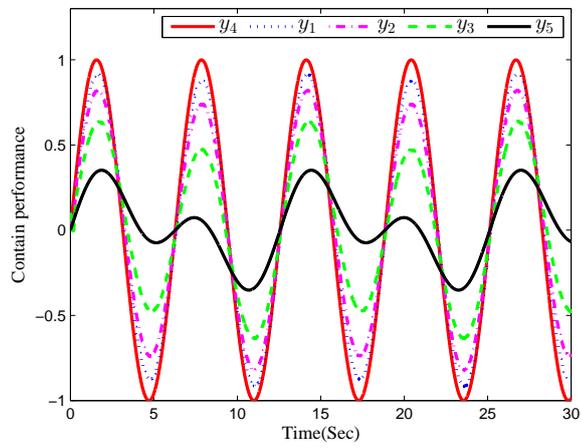


Fig. 9 Output of three followers and two leaders.

Table 2 Cases of  $c_{1,1}$  and  $c_{1,2}$ .

Case	Parameters
1	$c_{1,1} = 25, c_{1,2} = 5$
2	$c_{1,1} = 45, c_{1,2} = 15$
3	$c_{1,1} = 65, c_{1,2} = 25$

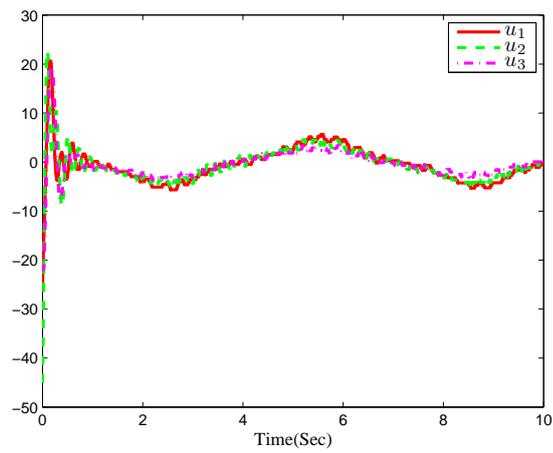


Fig. 10 Control inputs  $u_i$ ,  $i = 1, 2, 3$ .

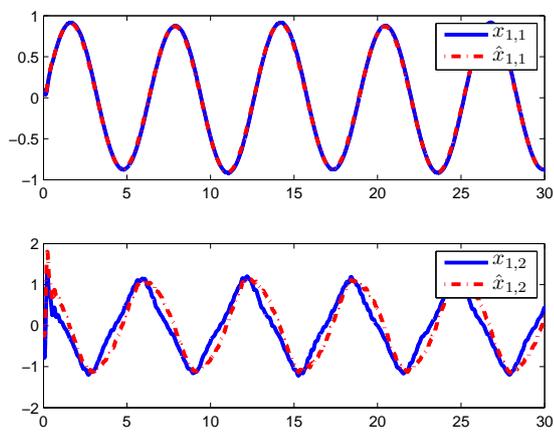


Fig. 11 States and their estimations for Follower 1.

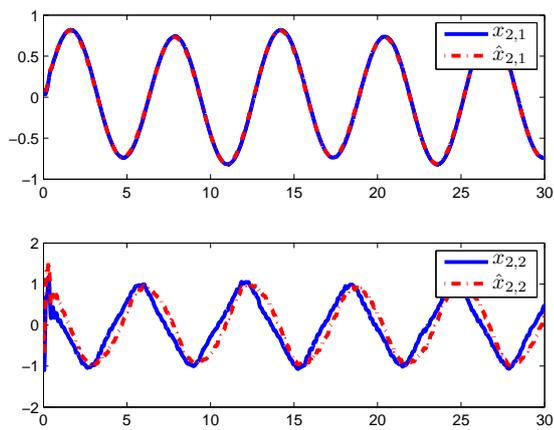


Fig. 12 States and their estimations for Follower 2.

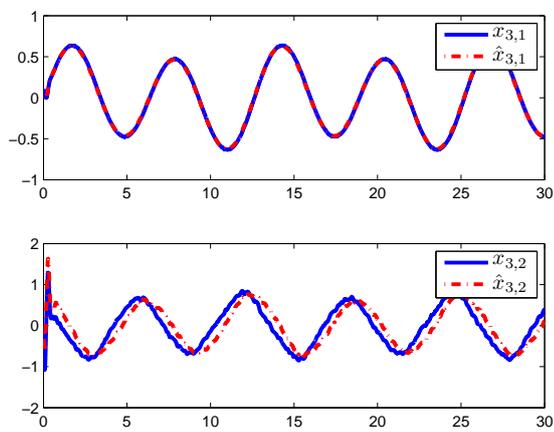


Fig. 13 States and their estimations for Follower 3.

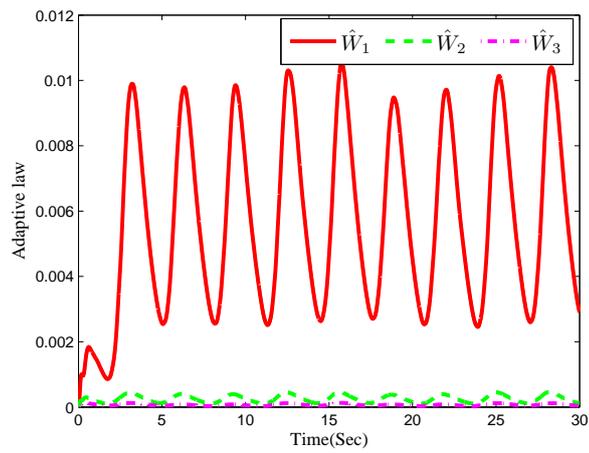


Fig. 14 Adaptive parameters.

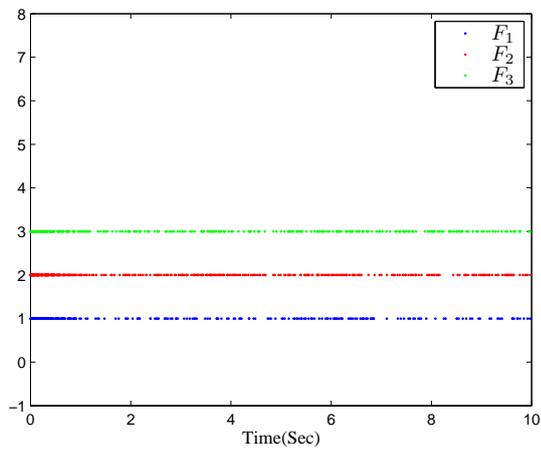
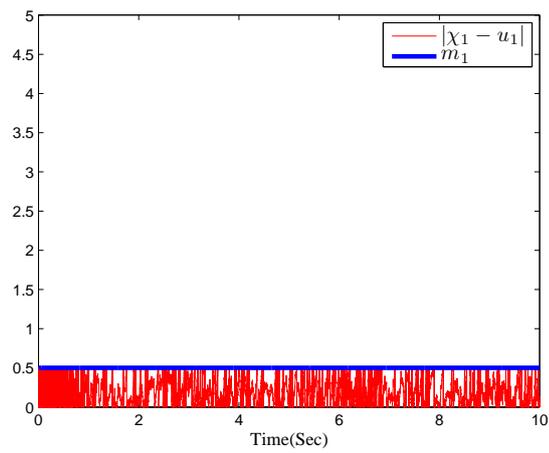
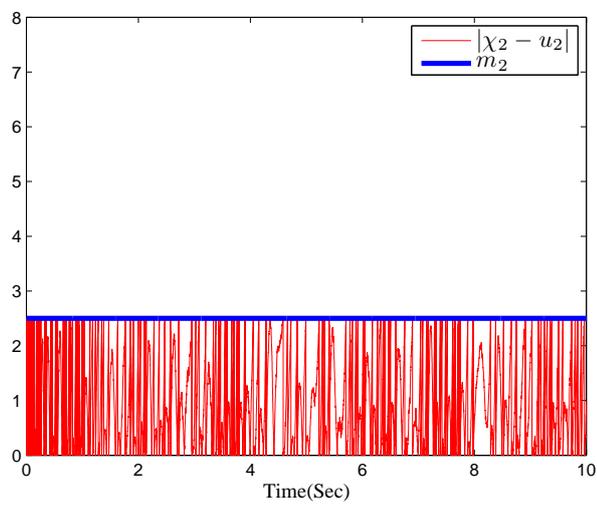


Fig. 15 Triggered instants of the three followers.



**Fig. 16** Curves of the triggered error and the threshold value as  $m_2$  is 0.5.



**Fig. 17** Curves of the triggered error and the threshold value as  $m_2$  is 2.5.

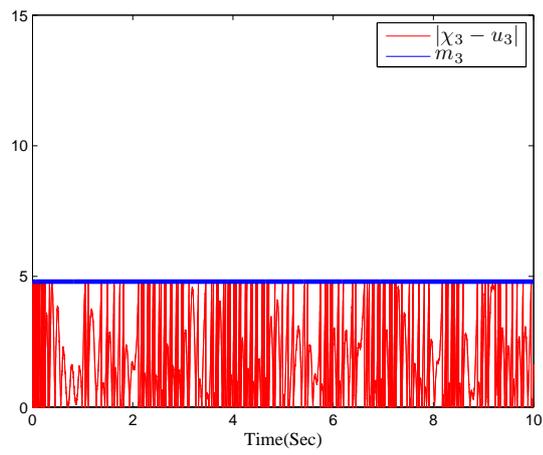


Fig. 18 Curves of the triggered error and the threshold value as  $m_2$  is 4.8.

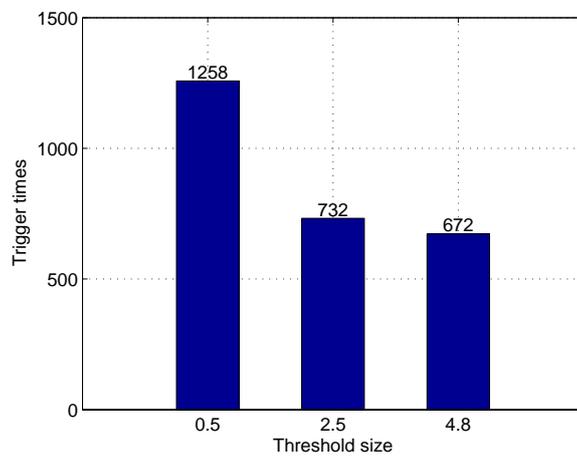


Fig. 19 Comparison of triggered number with different thresholds.

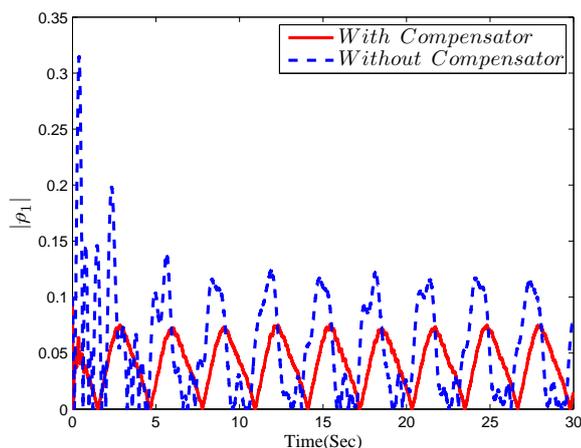


Fig. 20 Performance comparison of 1st follower with/without compensator.

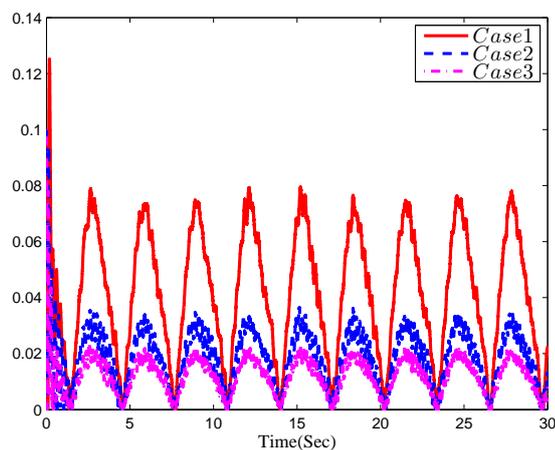


Fig. 21 Containment error with different parameters  $c_1$ .

## 387 5 Conclusion

388 A containment control strategy is proposed for a class of stochastic nonlinear  
 389 MASs based on event-triggered with fixed threshold. For unknown states of the  
 390 MAS, state observers are designed to reconstruct internal information. DSC  
 391 technology is used to improve the strategy of backstepping, and NNs estimate  
 392 unmodeled dynamics. For the purpose of reducing the resource occupation  
 393 of the network channel, an event-triggered strategy with fixed threshold is

394 designed to reduce the number of data transmission bits over the network  
395 channel. A Lyapunov function is developed to prove that all signals in the  
396 MASs are bounded in probability. The proposed control strategy is on the  
397 basis of fixed thresholds, where the threshold holds constant regardless of the  
398 magnitude of the control signal. This indicates that the result established in  
399 this paper is still far from a full investigation on the relation between triggered  
400 number and relative threshold as well as stochastic dynamics in individual  
401 followers, which is, therefore, worth our further research in the future.

#### 402 Declaration of interest

403 The authors declare no conflict interest.

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